

Chapter 8

DEFLECTION of STRUCTURES; Geometric Methods

¹ Deflections of structures must be determined in order to satisfy serviceability requirements i.e. limit deflections under *service* loads to acceptable values (such as $\frac{\Delta}{L} \leq 360$).

² Later on, we will see that deflection calculations play an important role in the analysis of statically indeterminate structures.

³ We shall focus on flexural deformation, however the end of this chapter will review axial and torsional deformations as well.

⁴ Most of this chapter will be a *review* of subjects covered in *Strength of Materials*.

⁵ This chapter will examine deflections of structures based on geometric considerations. Later on, we will present a more powerful method based on energy considerations.

8.1 Flexural Deformation

8.1.1 Curvature Equation

⁶ Let us consider a segment (between point 1 and point 2), Fig. 8.1 of a beam subjected to flexural loading.

⁷ The **slope** is denoted by θ , the change in slope per unit length is the **curvature** κ , the **radius of curvature** is ρ .

⁸ From *Strength of Materials* we have the following relations

$$ds = \rho d\theta \Rightarrow \frac{d\theta}{ds} = \frac{1}{\rho} \quad (8.1)$$

⁹ We also note by extension that $\Delta s = \rho \Delta \theta$

¹⁰ As a first order approximation, and with $ds \approx dx$ and $\frac{dy}{dx} = \theta$ Eq. 8.1 becomes

$$\kappa = \frac{1}{\rho} = \frac{d\theta}{dx} = \frac{d^2y}{dx^2} \quad (8.2)$$

¹⁴ Thus the slope θ , curvature κ , radius of curvature ρ are related to the y displacement at a point x along a flexural member by

$$\kappa = \frac{\frac{d^2y}{dx^2}}{\left[1 + \left(\frac{dy}{dx}\right)^2\right]^{\frac{3}{2}}} \quad (8.9)$$

¹⁵ If the displacements are very small, we will have $\frac{dy}{dx} \ll 1$, thus Eq. 8.9 reduces to

$$\kappa = \frac{d^2y}{dx^2} = \frac{1}{\rho} \quad (8.10)$$

8.1.2 Differential Equation of the Elastic Curve

¹⁶ Again with reference to Figure 8.1 a positive $d\theta$ at a positive y (upper fibers) will cause a *shortening* of the upper fibers

$$\Delta u = -y\Delta\theta \quad (8.11)$$

¹⁷ This equation can be rewritten as

$$\lim_{\Delta s \rightarrow 0} \frac{\Delta u}{\Delta s} = -y \lim_{\Delta s \rightarrow 0} \frac{\Delta\theta}{\Delta s} \quad (8.12)$$

and since $\Delta s \approx \Delta x$

$$\underbrace{\frac{du}{dx}}_{\varepsilon} = -y \frac{d\theta}{dx} \quad (8.13)$$

Combining this with Eq. 8.10

$$\frac{1}{\rho} = \kappa = -\frac{\varepsilon}{y} \quad (8.14)$$

This is the fundamental relationship between curvature (κ), elastic curve (y), and linear strain (ε).

¹⁸ Note that so far we made no assumptions about material properties, i.e. it can be elastic or inelastic.

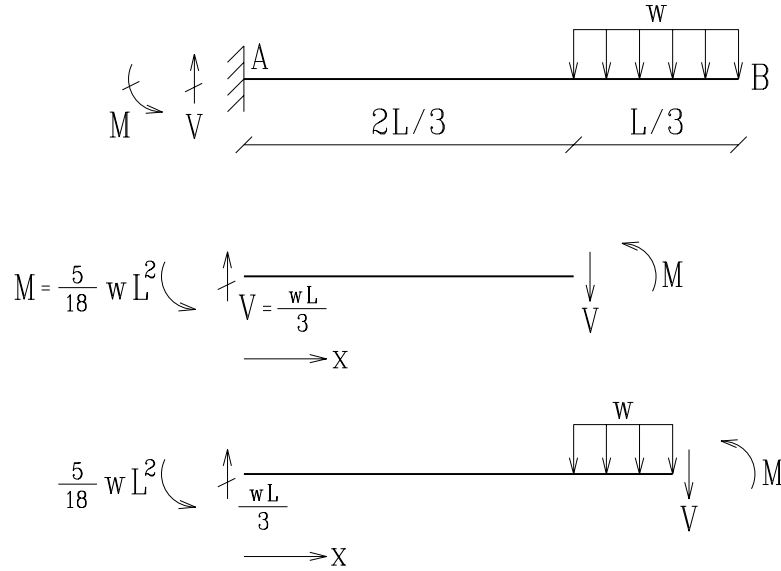
¹⁹ For the elastic case:

$$\left. \begin{aligned} \varepsilon_x &= \frac{\sigma}{E} \\ \sigma &= -\frac{My}{I} \end{aligned} \right\} \varepsilon = -\frac{My}{EI} \quad (8.15)$$

Combining this last equation with Eq. 8.14 yields

$$\frac{1}{\rho} = \frac{d\theta}{dx} = \frac{d^2y}{dx^2} = \frac{M}{EI} \quad (8.16)$$

This fundamental equation relates moment to curvature.



Solution:

At: $0 \leq x \leq \frac{2L}{3}$

1. Moment Equation

$$EI \frac{d^2 y}{dx^2} = M_x = \frac{wL}{3}x - \frac{5}{18}wL^2 \quad (8.22)$$

2. Integrate once

$$EI \frac{dy}{dx} = \frac{wL}{6}x^2 - \frac{5}{18}wL^2x + C_1 \quad (8.23)$$

However we have at $x = 0$, $\frac{dy}{dx} = 0$, $\Rightarrow C_1 = 0$

3. Integrate twice

$$EI y = \frac{wL}{18}x^3 - \frac{5wL^2}{36}x^2 + C_2 \quad (8.24)$$

Again we have at $x = 0$, $y = 0$, $\Rightarrow C_2 = 0$

At: $\frac{2L}{3} \leq x \leq L$

1. Moment equation

$$EI \frac{d^2 y}{dx^2} = M_x = \frac{wL}{3}x - \frac{5}{18}wL^2 - w(x - \frac{2L}{3})(\frac{x - \frac{2L}{3}}{2}) \quad (8.25)$$

2. Integrate once

$$EI \frac{dy}{dx} = \frac{wL}{6}x^2 - \frac{5}{18}wL^2x - \frac{w}{6}(x - \frac{2L}{3})^3 + C_3 \quad (8.26)$$

Applying the boundary condition at $x = \frac{2L}{3}$, we must have $\frac{dy}{dx}$ equal to the value coming from the left, $\Rightarrow C_3 = 0$

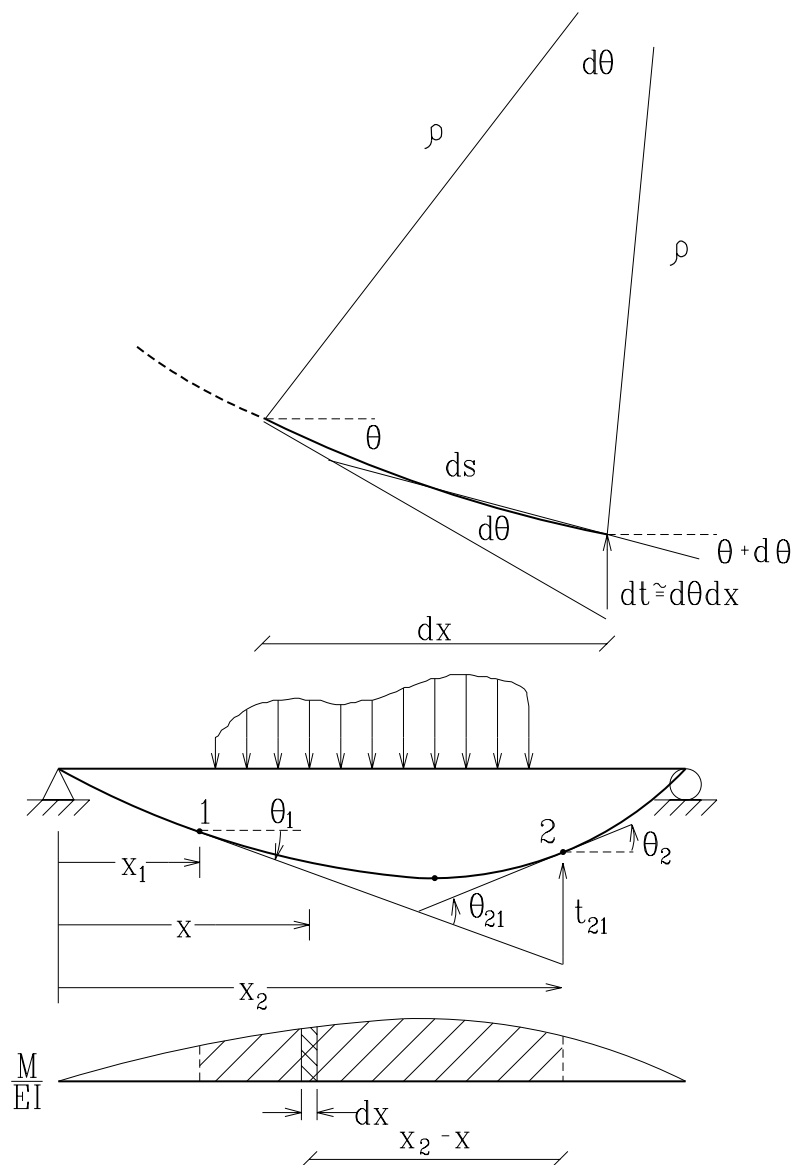


Figure 8.2: Moment Area Theorems